

On the Sweet Corrosion of Oil and Gas Wells

Yxuan Peng¹, Zhen Guo²

^{1,2}China University of Geosciences, 29 Xueyuan Rd, WuDaoKou, Haidian Qu, Beijing Shi, China

(²zhen.guo49@gmail.com)

Abstract- Sweet corrosion (CO_2) is one of the main concerns threatening the metallic infrastructures of oil industry. Downhole equipment of oil and gas wells are suffering more dramatically from CO_2 corrosion due to high temperature and high pressure (HTHP) exists in such conditions. In compare to the surface facilitates, corrosion of downhole equipment is more costly since the repair and/or replacement of the damaged parts requires total shutdown of the producing well. Indeed, the accessibility of downhole equipment is not as readily as surface equipment. Therefore, corrosion control program of oil and gas wells is very important for oil operators. This paper provides an overlook to the corrosion of oil wells and the important factors that govern corrosion in sweet environments.

Keywords- Sweet Corrosion, Oil well, HPHT, Downhole

I. INTRODUCTION

Corrosion is a real challenge for the metallic infrastructure of oilfields [1]-[4]. Carbon dioxide (CO₂) and hydrogen sulfide (H₂S) are two key players behind corrosion attacks in oil and gas production and transmission tubular [5]. Carbon dioxide (CO_2) corrosion is widely known as "sweet corrosion" while hydrogen sulfide (H₂S) corrosion is referred to "sour corrosion" [6], [7]. Downhole corrosion of oil and gas wells has taken considerable attention due to the high pressure & temperature, multiphase flow, complicated water chemistry, and high CO2 and H2S concentration in the produced streams that can cause corrosion failure of production tubing. Conditions in wells are often much harsher than those in the transportation lines [8]. The presence of oil can have a dramatic effect on the corrosion behavior of the system bases on the wettability characteristic of the crude oil. In addition, some surfactant present in crude oil can offer levels of corrosion inhibition if they reach the metal surface [2], [9]. In compare to surface facilities, prediction and mitigation of corrosion in downhole condition is a challenge for oil producers due to contribution of many important parameters in corrosion processes.

II. BASICS OF CO₂ CORROSION (SWEET CORROSION)

 CO_2 corrosion occurs in an aqueous environment. The aqueous phase plays the electrolyte role in the electrochemical reactions involved in corrosion processes. The metal exposed to such corrosive medium, in this case, mild carbon steel (iron), dissolves by the anodic reaction, and hydrogen gas

produced at steel surface as a result of hydrogen evolution (cathodic) reactions. Chemical and electrochemical reactions are contributing in corrosion phenomena. Important homogeneous chemical reactions taking place in the bulk solution in CO_2 environments are the followings:

Dissolution of carbon dioxide in water phase

$$\mathcal{CO}_{2(g)} \rightleftharpoons \mathcal{CO}_2 \tag{1}$$

Carbon dioxide hydration; formation of carbonic acid

$$CO_2 + H_2 O \rightleftharpoons H_2 CO_3 \tag{2}$$

Carbonic acid dissociation

$$H_2 C O_3 \rightleftharpoons H^+ + H C O_3^- \tag{3}$$

Bicarbonate anion dissociation

$$HCO_3^- \rightleftharpoons H^+ + CO_3^{2-} \tag{4}$$

Water dissociation

$$H_2 0 \rightleftharpoons H^+ + 0H^- \tag{5}$$

The main heterogeneous electrochemical (anodic and cathodic) reactions taking place at the steel surface are:

Anodic reaction; oxidation of iron

$$Fe_{(s)} \to Fe^{2+} + 2e^- \tag{6}$$

Cathodic hydrogen evolution; reduction of free hydrogen ions

$$2H^+ + 2e^- \to H_{2(g)} \tag{7}$$

Cathodic hydrogen evolution; reduction of carbonic acid

$$2H_2CO_3 + 2e^- \to 2HCO_3^- + H_{2(g)} \tag{8}$$

Cathodic hydrogen evolution; reduction of bicarbonate ions

$$2HCO_3^- + 2e^- \to 2CO_3^{2-} + H_{2(g)} \tag{9}$$

Cathodic hydrogen evolution; reduction of water

$$2H_20 + 2e^- \to 20H^- + H_{2(g)} \tag{10}$$

III. INFLUENTIAL PARAMETERS GOVERNING SWEET CORROSION IN OIL AND GAS WELLS

Pressure and temperature are important factors in the corrosion processes. Temperature is one of the main input parameters for corrosion prediction models including the de Waard-Milliams corrosion model [10]. Without a protective

corrosion product layer, high temperatures generally lead to higher corrosion rates, while low temperatures lead to lower corrosion rates. Iron carbonate (FeCO₃) is the main corrosion product layers in CO₂ environments [11]. Total pressure has little direct effect on the corrosion process but is directly affecting the partial pressures of CO₂ which, influence the corrosion rates. Pressure also affects the gas density and gas velocity. In high pressures and temperatures, both gas and liquid phases show non-ideal behaviors.

The volumetric flow rates of the produced stream including gas, oil and water are important parameters for calculating the velocity of each phase. Moreover, water velocity significantly influences the corrosion mechanism via mass transfer phenomena [5]. Moreover, erosion-corrosion accelerated in higher fluid velocities especially in presence of sand in the system. In high liquid velocities, possible removal of corrosion product exposes the bare steel surface to the corrosive medium and thus increases the chance of metal loss [12]. Corrosion rate is dramatically driving by the type of flow regime in well column [13], [14]. Flow can transition between several flow regimes during its travel form the down hole hole to the wellhead [17]. Generally, flow regime is strongly influenced by volumetric flow rate [15].

The composition of the gas stream has a significant effect on the corrosion, as it directly influences water composition. To predict the magnitude of corrosion, at least, the concentration of acidic gases (CO_2) should be measured in the gas phase. However, a more accurate characterization is possible if a thorough composition of gas phase is known.

The water chemistry of the brine co-produced along with the hydrocarbon is an important parameter for corrosion scenarios. The composition of the produced water influences the interaction between aqueous species and ionic strength of the solution. Brine contains different type of ions depending on well conditions. Table 1 shows a typical ion concentration seen in some oil wells in western Pennsylvania [16]. Ion type and concentration vary greatly form well to well even on the same oil reservoir.

 TABLE I.
 A TYPICAL ION TYPE AND CONCENTRATION OBSERVED IN OILFIELD BRINE

Sample name	Mg ²⁺	Ca ²⁺	Na ⁺	Cl
	(mg/L)	(mg/L)	(mg/L)	(mg/L)
1	2,000	16,000	56,700	122,000
2	2,500	18,000	58,300	123,000
3	2,520	19,000	58,500	123,000
4	2,410	17,100	52,100	111,000

It is reported that high concentrations of salts can lead to localized corrosion while it decreases general corrosion rate [17]. Brines in oilfield can have up to 200,000 ppm of chlorides, therefore, this ion needs to be taken into account for corrosion modeling [8], [16]. Chloride does not participate in electrochemical reactions involved in corrosion. However, it can destruct protective corrosion products on the steel surface and increase the mass transfer of corrosive species from bulk liquid phase towards the steel surface. Calcium is another ubiquitous ion present in oilfield brine, as shown in Table 1. Like chloride, calcium does not directly interfere the electrochemical reactions involved in corrosion. However, in presence of carbonate (CO_3^{2-}) and/or bicarbonate (HCO_3^{-}) ions, calcium carbonate can precipitate as solid phase if exceeding the solubility limits of CaCO_{3 (s)}. Precipitation of this scale (CaCO₃) can influence the mass transfer of corrosive species. The scaling tendency of a brine can be calculated if the ions concentration is known in the operational condition of the well [18], [19]. The acidity of the brine is often specified in terms of alkalinity, as a precise insitu pH measurement is almost impossible in down hole condition. Total alkalinity is the amount of acid requires neutralizing the produced water (brine) phase from the well. Alkalinity is typically measured in laboratory by means of titration method. The pH endpoint can vary depending on the procedure and the type of indicator employed, but typically it is between pH 4.6 and pH 6.5 [20]. This quantifies the acidreducing power of the produced water, and is generally reported as bicarbonate equivalent (HCO_3^-) . Total alkalinity is an important parameter in pH calculations.Organic acids may be present in oilfield brine. They can significantly impact the corrosion rate even at low concentrations [21].

The inner diameter of production tubing is used to convert the volumetric flow rates to velocities. The length of the tubing should be considered for temperature and pressure profiles prediction along the well column. The chemical and material properties of the tubing play a significant role in corrosion processes. Some researchers showed that different heat treatments (normalized, quenched, and tempered), metallurgy, and microstructures of carbon steel have an impact on the localized corrosion of carbon steels [22].

IV. CONCLUSIONS

In high pressure and temperature of oil and gas wells, production tubing is more susceptible to corrosion attacks. Material properties and the size of tubing influences the corrosion behavior of the tubing. Furthermore, Operational parameters including gas, oil, and water flow rate, flow regime, water chemistry of the brine, the composition of the gas phase, and pressure and temperature gradient along the well column have a significant impact on the corrosion mechanisms in down hole condition.

REFERENCES

- H. Mansoori, R. Mirzaee, A. H. Mohammadi, and F. Esmaeelzadeh, "Acid Washes, Oxygenate Scavengers Work Against Gas Gathering Failures," *OIL GAS J.*, vol. 111, no. 7, pp. 106–111, 2013.
- [2] M. Kermani and A. Morshed, "Carbon Dioxide Corrosion in Oil and Gas production _A Compendium," *Corrosion*, vol. 59, no. 8, pp. 659– 683, 2003.
- [3] H. Mansoori, R. Mirzaee, F. Esmaeelzadeh, and D. Mowla, "Altering CP Criteria Part of Unified Anti-SCC Approach," *Oil Gas J.*, vol. 111, no. 12, pp. 88–93, 2013.

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- [4] H. Mansouri, S. A. Alavi, R. Javaherdashti, H. Esmaeili, H. Mansouri, and A. Kariman, "pH effect microbial corrosion of Corten steel and Carbon steel in oily waste water with Pseudomonas Aeruginosa," *IOSR J. Eng.*, vol. 04, no. 01, pp. 28–32, 2014.
- [5] S. Nešić, "Key Issues Related to Modelling of Internal Corrosion of Oil and Gas Pipelines – A Review," *Corros. Sci.*, vol. 49, no. 12, pp. 4308– 4338, Dec. 2007.
- [6] H. Mansoori, D. Mowla, F. Esmaeelzadeh, and A. H. Mohammadi, "Case Study: Production Benefits from Increasing C-Values," *OIL GAS J.*, vol. 111, no. 6, pp. 64–69, 2013.
- [7] H. Mansoori, R. Mirzaee, and A. H. Mohammadi, "Pitting Corrosion Failures of Natural Gas Transmission Pipelines," presented at the International Petroleum Technology Conference, Beijing, China, 2013.
- [8] S. N. Smith and R. Pakalapati, "Thirty Years of Downhole Corrosion Experience at Big Escambia Creek: Corrosion Mechanisms and Inhibition," presented at the CORROSION 2004, 2004.
- [9] R. F. Weeter, "Downhole Corrosion Prevention and Treatment," presented at the International Petroleum Exhibition and Technical Symposium, 1982.
- [10] R. Nyborg, "CO2 Corrosion Models For Oil And Gas Production Systems," presented at the CORROSION 2010, 2010.
- [11] W. Sun and S. Nešic, "A mechanistic model of uniform hydrogen sulfide/carbon dioxide corrosion of mild steel," *Corrosion*, vol. 65, no. 5, pp. 291–307, 2009.
- [12] Y. Yang, B. Brown, Neš, S. Ic, M. E. Gennaro, and B. Molinas, "Mechanical Strength And Removal Of A Protective Iron Carbonate Layer Formed On Mild Steel In CO2 Corrosion," presented at the CORROSION 2010, 2010.

- [13] B. Bozzini, M. E. Ricotti, M. Boniardi, and C. Mele, "Evaluation of erosion–corrosion in multiphase flow via CFD and experimental analysis," *Wear*, vol. 255, no. 1–6, pp. 237–245, Aug. 2003.
- [14] S. Nešić, "Effects of Multiphase Flow on Internal CO2 Corrosion of Mild Steel Pipelines," *Energy Fuels*, vol. 26, no. 7, pp. 4098–4111, Jul. 2012.
- [15] H. Mansoori, V. Mobedifard, A. M. kouhpeyma, and A. H. Mohammadi, "Study Finds Simulation Flaws in Multiphase Environment," *Oil Gas J.*, vol. 112, no. 11, pp. 102–105, 2014.
- [16] P. E. Dresel and A. W. Rose, "Chemistry and Origin of Oil and Gas Well Brines in Western Pennsylvania," The Pennsylvania State University, Open-File Report OFOG 10–01.0, 2010.
- [17] H. Fang, "Low Temperature and High Salt Concentration Effects on General CO₂ Corrosion for Carbon Steel," Ohio University, 2006.
- [18] J. E. Oddo, M. B. Tomson, and others, "Why Scale Forms in the Oil Field and Methods to Predict It," SPE Prod. Facil., vol. 9, no. 01, pp. 47–54, 1994.
- [19] J. I. Al-Tammar, M. Bonis, H. Choi, and Y. M. Al-Salim, "Saudi Aramco Downhole Corrosion/Scaling Operational Experience and Challenges in HP/HT Gas Condensate Producers," *SAUDI ARAMCO J. Technol.*, 2014.
- [20] A. Hounslow, Water Quality Data: Analysis and Interpretation. CRC Press, 1995.
- [21] T. Tran, B. Brown, S. Nešić, and B. Tribollet, "Investigation of the Electrochemical Mechanisms for Acetic Acid Corrosion of Mild Steel," *CORROSION*, vol. 70, no. 3, pp. 223–229, Nov. 2013.
- [22] E. Akeer, B. Brown, and S. Nesic, "The influence of mild steel metallurgy on the initiation of localized CO2 corrosion in flowing conditions," presented at the CORROSION/2013, 2013, p. 2383.

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